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WINTER-16 EXAMINATION Model Answer

Subject code:

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Important Instructions to examiners:

- 1) The answers should be examined by key words and not as word-to-word as given in the model answer scheme.
- 2) The model answer and the answer written by candidate may vary but the examiner may try to assess the understanding level of the candidate.
- 3) The language errors such as grammatical, spelling errors should not be given more Importance (Not applicable for subject English and Communication Skills.
- 4) While assessing figures, examiner may give credit for principal components indicated in the figure. The figures drawn by candidate and model answer may vary. The examiner may give credit for any equivalent figure drawn.
 - 5) Credits may be given step wise for numerical problems. In some cases, the assumed constant values may vary and there may be some difference in the candidate's answers and model answer.
 - 6) In case of some questions credit may be given by judgement on part of examiner of relevant answer based on candidate's understanding.
 - 7) For programming language papers, credit may be given to any other program based on equivalent concept.



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| Q No. | Answer | marks |
|-------|--|-------|
| 1-A | Any 4 | |
| 1A-a | Sensible Heat: - Sensible heat is the heat that must be transferred to raise or | 1 |
| | lower the temperature of a substance or mixture of substance. | |
| | Heat capacity: It is the amount of heat required to increase the temperature of | 1 |
| | one gram of substance by one degree. | |
| 1A-b | Law of conservation of mass: It states that | 2 |
| | For any process input= output+accumulation | |
| 1A-c | Value of R: | 1 |
| | 1.987 Kcal/kmol.K | |
| | 8.315 J/mol.K | 1 |
| 1A-d | CO+2H ₂ →CH ₃ OH | 2 |
| | Stoichiometric coefficient of $CO:H_2 = 1:2$ | |
| 1 A-e | Law for real gas is | 1 |
| | Vander Waal's equation of state: | |
| | $(P+a/V^2)(V-b) = nRT$ | 1 |
| | Where a & b are constants | |
| 1A-f | Law of conservation of energy: | 1 |
| | Energy input= energy output + accumulation | 1 |
| 1-B | Any 2 | 12 |
| 1B-a | Basis: 100 kmoles of feed | |
| | A fed= 60 kmol | |
| | B fed=30 kmol | |
| | Inert fed = 10 kmol | |
| | Reaction is 2A+B→C | 2 |



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| Conversion of A =80% | | | | |
| A converted= (80/100) *6 | 60 = 48 kmol | | | |
| A unreacted= $60-48 = 12$ | kmol | | | |
| B reacted = 24 kmol | | | | |
| B unreacted = $30-24 = 6$ k | kmol | | | |
| C formed= 24 kmol | | | | 2 |
| Inert= 10 kmol | | | | |
| Composition of product | stream: | | | |
| component | kmol | Mol% | | |
| A | 12 | 23.07 | | |
| В | 6 | 11.54 | | |
| С | 24 | 46.15 | | 2 |
| Inert | 10 | 19.23 | | |
| total | 52 | | | |
| Basis: 1000 kg benzene-to 1000 Kg feed 28% benzene | | Distillate Xkg 52% benzene, | | 1 |
| 72% toluene Overall balance is | | Bottom product Y 5% benzene | kg | |
| 1000= X+ Y | | | | 1 |
| Benzene balance is | | | | |



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|------|--|----|
| | (28/100)* 1000 = 0.52 X + 0.05 Y | 1 |
| | Solving | |
| | X = 489.36kg and $Y = 510.64$ Kg | |
| | Distillate= 489.36kg | 2 |
| | Bottom product = 510.64 Kg | |
| | | |
| 1B-c | Basis: 1 Kg HCl acid | 1 |
| | $4HCl + O_2 \rightarrow 2Cl_2 + 2 H_2O$ | |
| | $HCl \ fed = 1/36.5 = 0.027 \ kmoles$ | 1 |
| | From reaction | |
| | Oxygen theoretically required = $0.027/4 = 6.85*10^{-3}$ | 1 |
| | % excess = 30 | |
| | Oxygen fed = $8.9*10^{-3}$ kmoles | 1 |
| | Air fed = 0.042 kmoles | 1 |
| | = 1.22 kg | 1 |
| | | |
| 2 | Any 4 | 16 |
| 2-a | Basis: 1000 Kg/hr HCHO formed | |
| | $CH_3OH \rightarrow HCHO + H_2$ | |
| | HCHO formed = 1000/ 30 = 33.33 kmole/h | 1 |
| | From reaction, CH ₃ OH reacted = 33.33 kmole/h | 1 |
| | Conversion = 65% | |
| | Conversion= (kmoles of CH ₃ OH reacted/kmoles of CH ₃ OH fed)* 100 | 1 |
| | Therefore CH ₃ OH fed = 51.28 | |
| | Feed rate of methanol= 51.28 * 32 kmol/h | |
| | = 1640.96 Kg/h | 1 |
| 2-b | Hess's law: | |
| | | |



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| | It states that the heat involved in a chemical reaction is same whether the | 2 |
| | reaction takes place in a single or in several steps. | |
| | A — ★ B ΔT1 | |
| | $B \longrightarrow C \Delta T2$ | 2 |
| | $C \longrightarrow D \Delta T3$ | |
| | $A \longrightarrow D \Delta T$ | |
| | Then | |
| | $\Delta T = \Delta T 1 + \Delta T 2 + \Delta T 3$ | |
| | | |
| 2-c | Basis: 4.73 kg coal | |
| | C+O ₂ →CO ₂ | |
| | At NTP, P= 101.325 KPa | |
| | T= 273 K | 1 |
| | PV=nRT | |
| | Or n= PV/RT | |
| | Moles of $CO_2 = 0.237$ kmoles | 1 |
| | Weight of $CO_2 = 0.237*44 = 10.428 \text{ kg}$ | |
| | Carbon in the sample = $(12/44)10.428 = 2.844 \text{ kg}$ | 1 |
| | Carbon content in the sample = $(2.844/4.73)100$ | |
| | = 60.13% | 1 |
| 2-d | Basis: 2000 kg wet solid | |
| | | 1 |
| | → Water Xkg | |
| | 2000 Kg feed | |
| | 70% solid dryer | |
| | | |
| | Product Y kg | |
| | | |



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| Overall balance is 2000 = X+ Y Balance for solid 0.70 * 2000 = 0.99 * Y Y = 1414.14 kg X = 585.86 Water removed = 585.86 kg Product obtained = 1414.14 kg 2-e Basis:15 kg propane Moles n= 15/44 = 0.341 kmoles At NTP, P= 101.325 KPa T= 273 K PV=nRT | 1 |
|---|----|
| 2000 = X+ Y Balance for solid 0.70 * 2000 = 0.99 * Y Y = 1414.14 kg X = 585.86 Water removed = 585.86 kg Product obtained = 1414.14 kg 2-e Basis:15 kg propane Moles n= 15/44 = 0.341 kmoles At NTP, P= 101.325 KPa T= 273 K | 1 |
| Balance for solid 0.70 * 2000 = 0.99 * Y Y = 1414.14 kg X = 585.86 Water removed = 585.86 kg Product obtained = 1414.14 kg 2-e Basis:15 kg propane Moles n= 15/44 = 0.341 kmoles At NTP, P= 101.325 KPa T= 273 K | 1 |
| 0.70 * 2000 = 0.99 * Y Y = 1414.14 kg X = 585.86 Water removed = 585.86 kg Product obtained = 1414.14 kg 2-e Basis:15 kg propane Moles n= 15/44 = 0.341 kmoles At NTP, P= 101.325 KPa T= 273 K | |
| Y = 1414.14 kg X = 585.86 Water removed = 585.86 kg Product obtained = 1414.14 kg 2-e Basis:15 kg propane Moles n= 15/44 = 0.341 kmoles At NTP, P= 101.325 KPa T= 273 K | |
| X = 585.86 Water removed = 585.86 kg Product obtained = 1414.14 kg 2-e Basis:15 kg propane Moles n= 15/44 = 0.341 kmoles At NTP, P= 101.325 KPa T= 273 K | 1 |
| Water removed = 585.86 kg Product obtained = 1414.14 kg 2-e Basis:15 kg propane Moles n= 15/44 = 0.341 kmoles At NTP, P= 101.325 KPa T= 273 K | |
| Product obtained = 1414.14 kg 2-e Basis:15 kg propane Moles n= 15/44 = 0.341 kmoles At NTP, P= 101.325 KPa T= 273 K | |
| 2-e Basis:15 kg propane Moles n= 15/44 = 0.341 kmoles At NTP, P= 101.325 KPa T= 273 K | 1 |
| Moles n= 15/44 = 0.341 kmoles At NTP, P= 101.325 KPa T= 273 K | |
| At NTP, P= 101.325 KPa T= 273 K | |
| T= 273 K | 1 |
| | 1 |
| PV=nRT | |
| | 1 |
| Or $V = nRT/P$ | |
| = 0.341* 8.314 * 273/101.325 | 1 |
| $= 7.64 \text{ m}^3$ | |
| 2-f Basis: 1 mol liquid C ₅ H ₁₂ | |
| $\Delta H^0_R = \Sigma \Delta H^0_{f(pr)} - \Sigma \Delta H^0_{f(react)}$ | 2 |
| = [(-393.51*5)+(-285.83*6)]- (-173.49) | |
| = -3509.04KJ | 2 |
| 3 Any 4 | 16 |
| 3-a Basis: Fixed mass of gas at at constant temperature | |
| Initial volume V1= 1m ³ | 1 |
| Initial pressure P1= P1atm | |
| Final volume V1= V2m ³ | |



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| | Final pressure P2= 1.85P1atm | 1 |
|-----|--|---|
| | P1V1/T1 = P2V2/T2 | 1 |
| | P1*1/T = 1.85P1*V2/T | |
| | $V2 = 0.5405 \text{ m}^3$ | 1 |
| | | |
| 3-b | Basis: 1 kmol methane gas | |
| | $Q = n[19.2494(T2-T1) + 52.1135*10^{-3}/2(T2^{2} - T1^{2}) + 11.973*10^{-6}/3 (T2^{3} - T1^{2}) + 11.973*10^{-6}/3 (T2^{3$ | 2 |
| | $T1^3$) - 11.3173 * $10^{-9}/4$ ($T2^4 - T1^4$) | |
| | $Q = 1[19.2494(523-303) + 52.1135*10^{-3}/2(523^2 - 303^2) + 11.973*10^{-6}/3 $ | 1 |
| | $523^3 - 303^3$) - 11.3173 * $10^{-9}/4$ ($523^4 - 303^4$) | |
| | = 4234.86 + 4735.03+459.9 - 187.84 | 1 |
| | = 9241.96 KJ | |
| | | |
| 3-c | Basis:100 kg coal | |
| | | |
| | →Burnt C Xkg | |
| | 1000 Kg feed | 1 |
| | 63% C burner | |
| | 24% ash | |
| | Refuse Y kg | |
| | 7% C, 93% ash | |
| | Component balance for ash | |
| | 24= 0.93 Y | 1 |
| | Or $Y = 25.80 \text{ Kg}$ | |
| | Balance for carbon | |
| | 63= X+ 0.07*25.80 | |
| | X= 61.194 Kg | 1 |
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|-----|---|----|
| | Unburnt carbon = 0.07*25.80 = 1.806 Kg | |
| | % of original C unburnt = (1.806/63)*100 | 1 |
| | = 2.867% | |
| | | |
| 3-d | | |
| | $N_2 + 3H_2 \longrightarrow 2NH_3$ | 1 |
| | $1 \text{ kmol } N_2 = 3 \text{ kmol } H_2$ | |
| | 25 " = ? | |
| | Molal flow rate of $H_2 = 75$ kmol/hr | 1 |
| | % conversion of $N_2 = (N2 \text{ reacted/ } N2 \text{ fed})*100$ | |
| | 25 = (N2 reacted/ 25)*100 | |
| | N_2 reacted = 6.25 kmol/h | 1 |
| | From reaction NH ₃ formed = 12.50 Kmol/h | |
| | $Kg NH_3 formed = 12.50 *17 = 212.5 Kg$ | 1 |
| 3-е | Basis: 1 kmol NH ₃ | |
| | $Q = n[Cpm2(T_2-T_0) - Cpm1(T_1-T_0)]$ | 2 |
| | $= 1[\ 37.\ 7063(422-298) - 35.8641(311-298)]$ | |
| | = 4209.35 KJ | 2 |
| 3-f | Basis: 100 kmol air | |
| | Avg. mol.wt of air = $M_1X_1+M_2X_2$ | 1 |
| | = 28 * 0.79 + 32 * 0.21 | |
| | = 28.84 | 1 |
| | Density = P* Mav / RT | 1 |
| | = 101.325 * 28.84/ 8.314 * 273 | |
| | $= 1.287 \text{ Kg/m}^3$ | 1 |
| 4 | Any 2 | 16 |
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|-----|---|---|---|
| 4-a | Basis: Mixture of N ₂ , CO ₂ , O ₂ | | |
| | Let X_1 , X_2 , X_3 be the mol fraction of N_2 , CO_2 , O_2 respectively. | 1 | |
| | 1st person 28 $X_1 + 44 X_2 + 32 X_3 = 30.08$ | 1 | |
| | 2^{nd} person 14 $X_1 + 44$ $X_2 + 32$ $X_3 = 30.08$ | 1 | |
| | $X_1 + X_2 + X_3 = 1$ | 1 | |
| | Solving the equations, we get | | |
| | $X_1 = 0.81$ | | |
| | $X_2 = 0.11$ | 2 | |
| | $X_3 = 0.08$ | | |
| | Volume % of $N_2 = 81\%$ | | |
| | Volume % of $CO_2 = 11\%$ | 2 | |
| | Volume % of $O_2 = 8\%$ | | |
| 4-b | Basis: Mixture of N ₂ , CO ₂ | | 1 |
| | $X_{CO2} = 1 - X_{N2}$ | | 1 |
| | Avg. mol.wt = $M_1X_1+M_2X_2$ | | 1 |
| | $31 = 28 X_{N2} + 44(1-X_{N2})$ | | |
| | Solving, $X_{N2} = 0.8125$ | | 2 |
| | $X_{CO2} = 0.1875$ | | |
| | Partial pressure of N_2 = Total pressure * mol.fr | | 1 |
| | = 101.325 * 0.8125 | | 2 |
| | = 82.33 KPa | | |
| 4-c | Basis: 100 kg flaked seeds | | |
| | Hexane+oil | | 1 |
| | | | |
| | seeds extractor | | 1 |
| | 18.6% oil, | | |
| | 69% solid cake Y kg0.8% oil, 87.7% solid | | |



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| | Component balance for solids | |
|-----|---|----|
| | 69 = 0.877 Y | 1 |
| | Or $Y = 78.68 \text{ Kg}$ | 1 |
| | Oil in cake = $(0.8/100)78.68$ | |
| | = 0.63 Kg | 1 |
| | Oil balance is | |
| | 18.6 = 0.63 + oil recovered | 1 |
| | Oil recovered = 17.97 kg | 1 |
| | % oil recovery = (17.97/18.6)* 100 = 96.61% | 1 |
| | | |
| 5 | Any 2 | 16 |
| 5-a | Basis : 100 Kg of coke Amount of carbon in coke = 0.9 x 100 = 90 Kg | |
| | Amount of $C = 90/12 = 7.5 \text{ katom}$ | 1 |
| | Reaction : $C + O_2> CO_2$ | |
| | From reaction , 1 katom $C = 1 \text{ kmol } O_2$ 12 Kg $C = 32 \text{ Kg } O_2$ 90 Kg $C = (32/12) \times 90 \text{ Kg } O_2$ | |
| | O_2 theoretically required = (32/12) x 90 = 240 Kg | |
| | O_2 theoretically required = $(240 \times 1000) / 32 = 7500 \text{ mol}$ | 1 |
| | Moles of O_2 theoretically required for 100 kg coke for complete combustion = 750 mol ans (a) | |
| | O_2 theoretically required = 240 / 32 = 7.5 kmol | 1 |
| | Air theoretically required = $7.5 * (100/21) = 35.71 \text{ kmol}$ | |
| | % excess | |



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|-----|--|--|---------------|-------|--------------|--|
| | Air actually supplied | = Air theoretically requi | | | | |
| | | 50 | 100 | | | |
| | Air actually supplied | = 35.71 x (1+) | = 53.57 kmol | | 1 | |
| | Air actually supplied | | | | | |
| | O_2 in air supplied = | = 53.57 x 0.21 = 11.25 k | rmol | | | |
| | N_2 in air supplied = | $53.57 \times 0.79 = 42.32 \text{ kg}$ | mol | | 1 | |
| | O_2 reacted for complete combustion of coke =7.5 kmol | | | | | |
| | Material Balance of | \mathbf{O}_2 | | | | |
| | O_2 in air supplied = | O ₂ reacted + O ₂ Unreac | cted | | 1 | |
| | O_2 Unreacted = 11.25 | 5 -7.5 =3.75 kmol | | | | |
| | CO_2 produced = $(1/1)$ x 7.5 = 7.5 kmol | | | | | |
| | Analysis of Gases at the end of Combustion: | | | | | |
| | Component | Quantity, Kmol | Mole% | | 2 | |
| | CO_2 | 7.5 | 14 | | | |
| | N_2 | 42.32 | 79 | | | |
| | O_2 | 3.75 | 07 | | | |
| | Total | 53.57 | 100 | | | |
| 5-b | Basis : 15000 mol/h | of N ₂ - H ₂ mixture | | | | |
| | Molal flow rate of gas | s mixture = 5 kmol/h | | | | |
| | $X N_2 = 25/100 = 0.25$ | | | | 1 | |
| | $X H_2 = 75/100 = 0.75$ | | | | | |
| | $C_P^o \text{ mix} = \Sigma C_P^o \text{ mix}$. $X i = X N_2$. $C_P^o N_2 + X H_2$. $C_P^o H_2$ = 0.25 (29.5909 -5.141x 10 ⁻³ T + 13.1829 x10 ⁻⁶ T ² - 4.968 x10 ⁻⁹ T ³) | | | | | |
| | $= 0.25 (29.5909 - 5.141x 10^{-3} T + 13.1829 x 10^{-1} - 4.968 x 10^{-1})$ + 0.75 (28.6105+1.0194 x 10 ⁻³ T - 0.1476 x 10 ⁻⁶ T ² +0.769 x 10 ⁻⁹ T ³) | | | | 2 | |



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| $= 28.8556 - 0.5207 \times 10^{-3} \text{ T} + 3.185 \times 10^{-6} \text{ T}^2 - 0.6652 \times 10^{-9} \text{ T}^3$ | | |
|--|---|---|
| Q = Heat added | | |
| $Q = n \square C^{o}p \text{ mix } dT$ T_{1} | | 1 |
| $Q = n \square [28.8556-0.5207 \times 10^{-3} \text{ T} + 3.185 \times 10^{-6} \text{T}^{2} \\ T_{1} \\ -0.6652 \times 10^{-9} \text{T}^{3}] \text{ dT}$ | | |
| 0.5207×10^{-3} = n [28.8556 (T2-T1) (T2 ² -T1 ²) 2 3.185×10^{-6} $+ (T23-T13) (T24-T14)]$ | | 2 |
| Where , n= 15 Kmol/h , $T_2 = 473$ K , $T_1 = 298$ K | | |
| 0.5207×10^{-3} = 15 [28.8556 (473 - 298) (473 ² - 298 ²) 2 $3.185 \times 10^{-6} \qquad 0.6652 \times 10^{-9}$ + (473 ³ - 298 ³) (473 ⁴ - 298 ⁴) |] | |
| Q = 15(5049.73 - 35.13 - 7.01) | | |
| Q = 76377.6 KJ/h = 21.216 kJ/s = 21.216 kW ans | | 2 |
| 5-c Basis: 1 Kg of petrol | | |
| Amount of H ₂ in petrol = 0.15 Kg, Amount of C in petrol = 0.85 kg | 5 | |



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| $H_2 + \frac{1}{2} O_2 \longrightarrow H_2O$ | 1 |
| $C + O_2 \longrightarrow CO_2$ | |
| From reactions : 1 kmol of $H_2 = 0.5$ kmol O_2 | |
| $2 \text{ kg of H}_2 = 16 \text{ kg O}_2$ | |
| 1 katom of $C = 1$ kmol O_2 | |
| $12 \text{ kg of C} = 32 \text{ kg O}_2$ | 1 |
| The rotical requirement of O_2 for $H_2 = 0.15 \times (16/2) = 1.20 \text{ Kg}$ | |
| The rotical requirement of O_2 for $C = 0.85 \times (32/12) = 2.27 \text{ Kg}$ | |
| Total therotical requriment of $O_2 = 1.20 + 2.27 = 3.47$ Kg | |
| Amount of air required for combustion = (3.47/0.23) =15.09 kg ans | 1 |
| (Air contais 23% O_2 and 77 % N_2 on weight basis) | |
| Amount of air supplied = 15.09 x 1.15 = 17.35 kg | |
| N_2 in supplied air = (0.77 x 17.35) /28 = 0.477 kmol | |
| O_2 in supplied air = $(0.23 \text{ x } 17.35)/32 = 0.125 \text{ kmol}$ | 1 |
| O_2 in dry product = $[0.23x(17.35-15.09)]/32 = 0.016$ kmol | |
| We have , $1 \text{ katom of } C = 1 \text{ kmol } CO_2$ | |
| (0.85/12) katom C = ? | 1 |
| $CO_2 \text{ produced} = (1/1) \text{ x}(0.85/12) = 0.071 \text{ kmol}$ | |
| The product flue gases contain CO ₂ , O ₂ and N ₂ | 1 |
| For ideal gases, Volume % = Mole % | |
| | |
| Composition of Dry Product Gases : | |
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| | Component | Quantity, Kmol | Mole% | | 2 |
|-----|--|--|--|----------|----|
| | CO_2 | 0.071 | 12.6 | | |
| | N_2 | 0.016 | 2.8 | | |
| | O_2 | 0.477 | 84.6 | | |
| | Total | 0.564 | 100 | | |
| 6 | Any 2 | | | | 16 |
| 6-a | Solve any TWO of t | he following | | | |
| | Waste acid, 55 % H Con.nitric acid 90% HNO ₃ Con.sulphuric acid 95% H ₂ SO ₄ | H ₂ SO ₄ ,20% HNO ₃ lending | Desired mi 00 kg H ₂ SO ₄ , 26% HNO ₃ | xed acid | 1 |
| | | kg of waste acid ,concentricid to make 1000 kg desire | | and | 1 |
| | Overall material Balance: | | | | |
| | X+Y+Z=1000(1) | | | | 1 |
| | Material Balance Of H ₂ SO ₄ | | | | |
| | 0.55X + 0.95 Y = 0.60 |) x 1000 | | | |
| | 0.55X + 0.95 Y = 600 |) | | | |
| | 600 – 0.55 X | | | | |
| | Y= | | | | |



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|-----|--|------------|
| | 0.95 | 1 |
| | Y = 631.58 - 0.58 X - (2) | |
| | Material Balance Of HNO ₃ | |
| | $0.2X + 0.90 Z = 0.26 \times 1000$ | |
| | 0.2X + 0.95Y = 260 | |
| | 260 - 0.2 X | |
| | Z = | |
| | 0.90 | |
| | Z = 288.9 - 0.222 X - (3) | 1 |
| | Putting values of Y and Z in equation (1) from (2) and (3) and solve for X | |
| | X + (631.58-0.58 X) +(288.9 -0.222 X) =1000 | |
| | 0.198 X = 79.52 | 1 |
| | X = 401.6 kg | |
| | We have $Y = 631.58 - 0.58 X$ | |
| | $Y = 631.58 - 0.58 \times 401.6 = 398.65 \text{ Kg}$ | 1 |
| | We have $Z = 288.9 - 0.222 \text{ X}$ | |
| | $Z = 288.9 - 0.222 \times 401.6 = 199.75 \text{ Kg}$ | |
| | Waste acid = 401.6 kg | |
| | Concentrated sulphuric acid = 398.65 kg | |
| | Concentrated nitric acid = 199.75 kg | |
| 6-b | Basis: 1 Kmol /h benzene fed to reactor | |
| | Benzene, HNO ₃ , H ₂ SO ₄ → Reactor | |
| | → Product stream NB, DNB, HNO ₃ etc | |
| | | |



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| $\mathrm{H}_{2}\mathrm{SO}_{4}$ | |
|---|--|
| Reaction 1: $C_6H_6 + HNO_3 - C_6H_5NO_2 + H_2O$ | |
| $ m H_2SO_4$ | |
| Reaction 2: $C_6H_5NO_2 + HNO_3 - C_6H_4(NO_2)_2 + H_2O$ | |
| Benzene reacted = $0.9 \times 1 = 0.9 \text{ kmol/h}$ | |
| Let X be the dinitrobenzene formed per hour | |
| (kmol nitrobenzene /h) / (kmol dinitrobenzene /h) = 17/1 | |
| Nitrobenzene produced = 17 x kmol | |
| From reaction 1 and 2 | |
| 1 kmol of $C_6H_6 = 1$ kmol of $C_6H_5NO_2$ | |
| = 1 kmol of $C_6H_4(NO_2)_2$ | |
| Benzene reacted to produce nitrobenzene = $(1/1) \times 17 \times \text{kmol/hr}$ | |
| Benzene reacted to dinitrobenzene = $x \text{ kmol}$ | |
| Benzene reacted = $0.9 = 17 x + x$ | |
| x = 0.05 kmol/hr | |
| Nitrobenzene produce = $17(0.05) = 0.85 \text{ kmol/h}$ | |
| $1 \text{ kmol of } C_6H_6 = 1 \text{ kmol } HNO_3$ | |
| Stoichometric requriment of nitric acid for | |
| 1 kmol benzene /h = $1/1 \times 1 = 1 \text{ kmol/h}$ | |
| | |
| Nitric acid fed to reactor = 1 [$1 + (65/100)$] = 1.65 kmol/h | |
| Nitric acid fed to reactor = $1.65 \times 63 = 104.95 \text{ kg/h}$ | |
| Nitrobenzene produce = $17(0.05) = 0.85 \times 123 = 104.55 \text{ kg/h}$ | |
| Benzene fed to reactor = 1 x 78 = 78 kg/hr | |
| | |
| Nitric acid fed to reactor fed to produce of 2000 kg/hr of nitrobenzene = | |
| $(103.95/104.55) \times 2000 = $ 1988.5 kg/hr | |



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|---|-----|--|----------------------------|---|
| | | Benzene fed to reactor fed to produce of 2000 kg/hr of nitrobenzene = (78/104.55) x 2000 = 1492.1kg/hr | 1 | |
| 6 | 5-с | Basis: One day of operation | 1 | |
| | | Wet solids handled = 1000 kg | | |
| | | Let X be the Kg of product obtained from first dryer and Y be the Kg of water removed in first dryer. | | |
| | | Material Balance of solids over First Dryer : | | |
| | | 0.50 * 1000 = 0.80 * X | 1 | |
| | | X = 625 Kg | | |
| | | Overall Material Balance over First Dryer : | | |
| | | X + Y = 1000 | | |
| | | 625 + Y = 1000 | 1 | |
| | | Y= 375 Kg Input to second dryer is 625 Kg of wet solid containing 20% moisture Material Balance of solids over Second Dryer: | 1 | |
| | | 0.8 * 625 = 0.98 * Z | | |
| | | Z = 510.20 Kg | | |
| | | Weight of final product = 510.20 Kg ans. (b) | | |
| | | Overall Material Balance over Second Dryer : | 2 | |
| | | 625 = 510.20 + Water removed | | |
| | | | | |

Water removed in second dryer = 625-510.20 = 114.8 Kg



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| Water in wet solids fed to first dryer =0.5 * 1000 = 500 Kg | 1 |
|---|---|
| % of original water removed in first dryer | |
| = (375/500) *100 = 75 % | |
| % of original water removed in Second dryer | 2 |
| = (114.8/500) *100 = 22.96 % | |
| % of original water removed in first dryer = 75 % | |
| % of original water removed in Second dryer = 22.96 % | |
| ans. (a) | |
| | |